Attorney Docket No: NAVI-009/02US

the specification of which:

PATENT

DECLARATION

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

- -	···· op ·		
		[X] is attached he	ereto.
1111		[] was filed on	, and identified as Attorney Docket No. NAVI-009/02US.
i.		[] was filed on	, as Application Serial No.
= 	and		
3		[] the amendmen	t(s) of which were filed on .
1	specifi	•	t I have reviewed and understand the contents of the above-identified ne claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to the patentability of this application in accordance with Title 37, Code of Federal Regulations, Section 1.56.

I hereby claim foreign priority benefits under title 35, United States Code, Section 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s) (Country) (Number) (Day/Month/Year Filed	Priority Claimed (Yes/No)
**	Yes
• • • • • • • • • • • • • • • • • • •	Yes

I hereby claim the benefit under Title 35, United States Code, § 119(e) of any United States provisional application(s) listed below.

60/100,290	September 14, 1998
(Application Number)	(Filing Date)
60/100,224	September 14, 1998
(Application Number)	(Filing Date)
60/109,232	November 18, 1998
(Application Number)	(Filing Date)
60/109.234	November 18, 1998
(Application Number)	(Filing Date)

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, Section 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, Section 1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application:

Appl. Ser. No.

Filing Date

Status (Pat'd./Pend./Aband.)

I direct that correspondence concerning this application be directed to

COOLEY GODWARD LLP
Attention: Patent Group
Five Palo Alto Square
3000 El Camino Real
Palo Alto, California 94306-2155
Telephone (650) 843-5000.
Facsimile (650) 857-0663

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Full name of sole or First inventor: Grass, George M.				
Inventor's signature	DateDate			
Residence:	Tahoe City, California			
Citizen of:	United States of America			
Post Office Address:	1506 Juniper Mountain Road, P.O. Box 1242 Tahoe City, California 96145			
Full name of sole or Second inver	ntor: Leesman, Glen D.			
Inventor's signature	Date 05/10/89			
Residence:	Hamilton, Montana			
Citizen of:	United States of America			
Post Office Address:	186 Nighthawk Lane Hamilton, Montana 59840-9307			
Full name of sole or Third invent	or: Nortis, Daniel A.			
Inventor's signature	Date 5/7/99			
Residence:	San Diego, California			
Citizen of:	United States of America			
Post Office Address:	3145 Cowley Way, #130 San Diego, California 92117			
Full name of sole or Fourth inven	ator: Sinko, Patrick J.			
Inventor's signature	Date 5/10/99			
Residence:	Lebanon, New Jersey			
Citizen of:	United States of America			
Post Office Address:	2 Country Place Lebanon, New Jersey 08833			

Full name of sole or Fifth in	ventora Wehrli, John E.
Inventor's signature	Date 5/7/99
Residence:	Mountain View, California
Citizen of:	United States of America
Post Office Address:	1879 Springer Unit B

CONFIDENTIAL

Attorney Docket No: NAVI-009/02US

PATENT

Express Mail Label Number:

EM 570 539 405 US

Date of Deposit:

May 26, 1999

I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, DC 20231.

Date

26 May 99

By

VLADIMIR SKLIBA

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re application of George M. Grass, et al.

Serial No.:

Not yet assigned

Examiner:

Not yet assigned

Filed:

Herewith

Art Unit:

Not yet assigned

For:

METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

Assistant Commissioner for Patents BOX PATENT APPLICATION Washington, D.C. 20231

POWER OF ATTORNEY BY ASSIGNEE AND EXCLUSION OF INVENTORS UNDER 37 CFR 1.36 AND 3.71

Sir:

The undersigned assignee of the entire interest in the application for Letters Patent identified above hereby revokes all prior appointments of attorneys and appoints

Nina M. Ashton	37,273	Marcella Lillis	36,583
Alexandra J. Baran	39,101	Tom M. Moran	26,314
James A. Bradburne	38,389	Richard L. Neeley	30,092
Aaron S. Brodsky	39,920	Craig P. Opperman	37,078
Shelley P. Eberle	31,411	Marya A. Postner	42,085
Richard M. Goldman	25,585	Gurjeev K. Sachdeva	37,434
Willis E. Higgins	23,025	William E. Winters	42,232
Peter R. Leal	24,226	Kevin J. Zimmer	36,977

all of the firm of Cooley Godward LLP, to prosecute this application and to transact all business in the United States Patent and Trademark Office connected therewith. This appointment shall be to the exclusion of the above-identified inventor(s) and any attorney(s) appointed by such inventor(s), in accordance with the provisions of 37 C.F.R. 1.36 and 3.71.

Assignee's rights are evidenced by an assignment

- [X] a copy of which is enclosed herewith.
- [] previously recorded on at reel, frame(s).

Please direct all telephone calls and correspondence to:

Cooley Godward LLP Attention: Patent Group Five Palo Alto Square 3000 El Camino Real Palo Alto, CA 94306-2155 Telephone: 650-843-5000

Facsimile: 650-857-0663

Assignee: Navievte, Inc.
Signature:
Name: John K. Wehrli, Esq.
Title: Senior Director, Legal Affairs/ Corporate Secretary
Address: 9880 Campus Point Drive, San Diego, California 92121
Date: May 14, 1999

CONFIDENTIAL

Attorney	Docket	No:	NAV	/I-0	09/	02US
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PATENT

Express Mail Label Number:

EM 570 539 405 US

Date of Deposit:

May 26, 1999

I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, DC 20231.

Date

26 May 99

Bv

VLADIMIR SKLIBA

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re application of George M. Grass, et al.

Serial No.:

Not yet assigned

Examiner:

Not yet assigned

Filed:

May 26, 1999

Art Unit:

Not yet assigned

For:

METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES.

Assistant Commissioner for Patents Washington, D.C. 20231

STATEMENT UNDER 37 CFR 3.73(b) ESTABLISHING RIGHT OF ASSIGNEE TO TAKE ACTION

The assignee(s) of the entire right, title and interest hereby seek(s) to take action in the PTO in this matter.

IDENTIFICATION OF ASSIGNEE

Name of Assignee:	Navicyte, Incorporated	
Type of Assignee:	Corporation	

PERSON AUTHORIZED TO SIGN

Name of Person Authorized to Sign: James A. Brad	burne, Ph.D.			
Title of Person Authorized to Sign: Agent of Record				
[X] I, the person signing below, state that I am empowered to sign this statement on behalf of the assignee.				
BASIS OF ASSIGNEE'S INTER	EST			
Ownership by the assignee is established as follows. A charto the current assignee is shown below:	in of title from the inventor(s)			
1. From: <u>George M. Grass, Glen D. Lee</u> Patrick J. Sinko and John E. Wehrli	esman, Daniel A. Norris,			
To: Navicyte, Incorporated				
Recordation Date: <u>12/22/98</u> Reel: <u>9673</u>	Frame: <u>0774-0777</u>			
[] Copies of the documents in the chain of title are attached	ched.			
Attn: Patent Group Five Palo Alto Square 3000 El Camino Real Palo Alto, CA 94306-2155 Tel: (650) 843-5000 Fax: (650) 857-0663 By:	Respectfully submitted, COOLEY GODWARD LLP James A. Bradburne, Ph.D. Reg. No. 38,389			

PATENT APPLICATION

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re the Application of:

GRASS et al.

Art Unit: 1631

Application No.: 09/320,069

Examiner: M. Moran

Filed: May 26, 1999

Attorney Dkt. No.: 109904-00027

For: METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

REVOCATION OF POWER OF ATTORNEY AND NEW APPOINTMENT

Assistant Commissioner for Patents Washington, D.C. 20231

November 5, 2001

Sir:

Dr. Christian Kilger, the undersigned, certifies that Lion Bioscience AG is the assignee of the entire right, title and interest in U.S. Patent Application Serial No. 09/320,069, filed May 26, 1999, by virtue of an assignment from NaviCyte, Inc., a copy of which is attached hereto. The assignment to NaviCyte was recorded in the Patent and Trademark Office at Reel 9673, Frame 0774-0777 on December 22, 1998.

Further, Lion Bioscience AG, as assignee of the entire interest in and to the above-identified United States patent application hereby revokes all powers of attorney previously given and appoints Arent Fox Kintner Plotkin & Kahn, 1050 Connecticut Avenue, Suite 600, Washington, DC, 20036-5339, a firm composed of:

Charles M. Marmelstein, Reg. No. 25,895; Robert B. Murray, Reg. No. 22,980; George E. Oram, Jr., Reg. No. 27,931; Douglas H. Goldhush, Reg. No. 33,125; Richard J. Berman, Reg. No. 39,107; Murat Ozgu, Reg. No. 44,275; Robert K. Carpenter, Reg. No. 34,794; Gregory B. Kang, Reg. No. 45,273; Rustan Hill, Reg. No. 37,351; Kevin F. Turner, Reg. No. 43,437; Rhonda C. Barton, Reg. No. P47,271 and Hans J. Crosby, Reg. No. 44,634, Brian A. Tollefson, Reg. No. 46,338, Lynn D. Anderson, Reg. No. 46,412, David D. Dzara, Reg. No. 47,543; Laurence J. Edson, Reg. No. 44,666; Michael A. Steinberg, Reg. No. 43,160; and Lynn A. Bristol, Reg. No. 48,898.

as principal attorneys to prosecute said application and to transact all business in the Patent and Trademark Office connected therewith.

The undersigned has reviewed all of the appropriate documents and, to the best of the undersigned's knowledge and belief, title is in the assignee identified above.

The undersigned (whose title is supplied below) is empowered to sign this paper on behalf of the assignee.

By the provisions of 28 U.S.C. §1746, I hereby declare under penalty of perjury under the laws of the United States of America that the foregoing is true and correct.

Executed on: November 5, 2001

(date)

Name:

Dr. Christian Kilger

Title:

Director of IP and Licensing

Signature

ATTACHED SHEET

U.S. Patent 5,183,760

U.S. Patent 5,591,636

U.S. Serial Number 09/320,069

U.S. Serial Number 09/320,270

U.S. Serial Number 09/320,545

U.S. Serial Number 60/224,106

U.S. Patent 5,599,688

U.S. Patent 6,146,883

U.S. Serial Number 09/320,372

U.S. Serial Number 09/320,371

U.S. Serial Number 09/320,544

<u>ASSIGNMENT</u>

WHEREAS, NaviCyte, Inc. (hereinafter ASSIGNOR) a company having its principal office and place of business at Sparks, Nevada, USA owns the inventions, and the patents and patent applications in various countries directed thereto, as set forth on the 2 page attachment hereto.

AND, WHEREAS, LION Bioscience AG (hereinafter ASSIGNEE), a company having its principal office and place of business at Heidelberg, Germany, is desirous of acquiring all interest therein.

NOW, THEREFORE, in consideration of One Dollar (\$1.00) and other good and valuable consideration, the receipt and sufficiency of which are hereby acknowledged, the above said ASSIGNOR by these presents does sell, assign and transfer unto the said ASSIGNEE, its successors, assigns and legal representatives, the full and exclusive right, title and interest in and to the said inventions in the United States and other countries including the ful and extensive right, title and interest world-wide in and to the patents and patent applications on the attachment hereto.

NaviCyte, Inc.

Title:

Date:

Mitness:

APPENDICIES

Appendix 1: Abbreviation Key for Mass-Volume Model

Abbreviation			
Kf sd = associated rate constant for stomach and duodenum			
Ka dj = associated rate constant for duodenum and jejunum			
Ka ji = associated rate constant for jejunum and ileum			
Ka ie = associated rate constant for ileum and colon			
Ka co = associated rate constant for colon and excretion			
SD trans = transfer rate between stomach and duodenum			
DJ trans = transfer rate between duodenum and jejunum			
JL trans = transfer rate between jejunum and ileum			
IC trans = transfer rate between ileum and colon			
Waste = transfer rate between colon and excretion			
pH s = pH stomach			
pH s2 = pH duodenum			
pH s3 = pH jejunum			
pH s4 = pH ileum			
pH s5 = pH colon			
sol profile = solubility profile for stomach			

sol profile 2 = solubility profile for duodenum
sol profile 3 = solubility profile for jejunum
sol profile 4 = solubility profile for ileum
sol profile 5 = solubility profile for colon
stom ka = associated rate constant for stomach compartments 1 and 2
duo ka = associated rate constant for duodenum compartments 1 and 2
Jej ka = associated rate constant for jejunum compartments 1 and 2
Il ka = associated rate constant for ileum compartments 1 and 2
Colon ka = associated rate constant for colon compartments 1 and 2
SA stom = surface area of stomach
SA duo = surface area of duodenum
SA jej = surface area of jejunum
SA il = surface area of ileum
SA colon = surface area of colon
Perm stom = permeability of stomach
Perm duo = permeability of duodenum
Perm jej = permeability of jejunum
Perm il = permeability of ileum
Perm colon = permeability of colon

Ka sd = associated rate construct for stomach fluid absorption

Ka du = associated rate construct for duodeunm fluid absorption

Ka je = associated rate construct for jejunm fluid absorption

Ka il = associated rate construct for ileunm fluid absorption

Ka co = associated rate construct for colon fluid absorption

Note: other abbreviations adhere to above descriptors and are self explanatory

Appendix 2: Equations, Parameters and Values For Mass-Volume Model

```
amt_plasma(t) = amt_plasma(t - dt) + (trans_21 + ka - elimination - trans_12) * dt
     INIT amt plasma = 0
     INFLOWS:
     trans_21 = k21*comp_2
     ka = tot_abs_rate
     OUTFLOWS:
     elimination = amt plasma*k elim
     trans_12 = k12*amt plasma
     blood_side_col(t) = \overline{b}lood_side_col(t - dt) + (colon_ka_5) * dt
     INIT blood side col = 0
INFLOWS:
colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
    ELSE Vol_colon*sol_profile_5*SA_colon*perm_colon*3600
Ф
    blood_side_dou(t) = blood_side_dou(t - dt) + (duo_ka) * dt
₫
Ū
    INIT blood side dou = 0
Ш
    INFLOWS:
Ш
    duo ka
                         IF
                                 Vol duod*sol profile 2
                                                                      duodenum
                                                                                      THEN
    duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
ᆣ
<u>_</u>
    blood\_side\_il(t) = blood\_side\_il(t - dt) + (Il ka) * dt
N
    INIT blood side il = 0
H
    INFLOWS:
    Il_ka = IF Vol_ileum*sol_profile_4 >=Ileum THEN Ileum*SA_Il*perm_Il*3600
                                                                                       ELSE
    Vol_ileum*sol_profile 4*SA II*perm II*3600
    blood_side_jej(t) = blood_side_jej(t - dt) + (Jej ka) * dt
    INIT blood side jej = 0
    INFLOWS:
    Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
    Vol_jej*sol_profile_3*SA jej*perm jej*3600
    blood\_side\_sto(t) = blood\_side\_sto(t - dt) + (stom\_ka) * dt
    INIT blood side sto = 0
    INFLOWS:
   stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
   ELSE Vol_stom*sol_profile*SA stom*perm stom*3600
   Colon(t) = Colon(t - dt) + (IC trans - Waste - colon ka 5) * dt
   INIT Colon = 0
```

```
INFLOWS:
    IC trans = ka ic*Ileum
    OUTFLOWS:
    Waste = ka col*Colon
    colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
    ELSE Vol_colon*sol_profile_5*SA colon*perm colon*3600
    comp 2(t) = comp \ 2(t - dt) + (trans \ 12 - trans \ 21) * dt
    INIT comp 2 = 0
    INFLOWS:
    trans 12 = k12*amt_plasma
    OUTFLOWS:
    trans_21 = k21*comp_2
    duodenum(t) = duodenum(t - dt) + (SD_trans - duo_ka - DJ_trans) * dt
   INIT duodenum = 0
INFLOWS:
SD_trans = if Stomach > 0 then kf_sd*Stomach else 0
Ð
☐ OUTFLOWS:
₩ duo_ka
                       IF
                                Vol duod*sol profile 2
                                                                    duodenum
                                                                                    THEN
duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
    DJ_trans = ka dj*duodenum
   excretion(t) = excretion(t - dt) + (vol cw) * dt
   INIT excretion = 0
ΠJ
   INFLOWS:
   vol cw = Vol colon*ka col
   excretion_2(t) = excretion_2(t - dt) + (Waste) * dt
   INIT excretion 2 = 0
   INFLOWS:
   Waste = ka col*Colon
   Ileum(t) = Ileum(t - dt) + (JL_trans - IC_trans - Il_ka) * dt
   INIT Ileum = 0
   INFLOWS:
   JL_trans = ka ji*Jejunum
   OUTFLOWS:
   IC trans = ka ic*Ileum
   Il_ka = IF Vol_ileum*sol_profile_4 >=Ileum THEN Ileum*SA_Il*perm Il*3600
                                                                                    ELSE
   Vol_ileum*sol profile 4*SA Il*perm Il*3600
   Jejunum(t) = Jejunum(t - dt) + (DJ trans - JL trans - Jej ka) * dt
```

```
INIT Jejunum = 0
     INFLOWS:
     DJ_trans = ka_dj*duodenum
     OUTFLOWS:
     JL_trans = ka ji*Jejunum
    Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
    Vol_jej*sol_profile_3*SA_jej*perm_jej*3600
    serosal\_col(t) = serosal\_col(t - dt) + (Adsorp\_col - col\_secretion) * dt
    INIT serosal col = 0
    INFLOWS:
    Adsorp\_col = PULSE(1.67,0,.1) + 0*Vol\_colon*ka\_co
    OUTFLOWS:
    col_secretion = 0
    serosal\_dou(t) = serosal\_dou(t - dt) + (Adsorp\_Duo - duo\_secretion) * dt
INIT serosal_dou = 0
    INFLOWS:
U
    Adsorp_Duo = PULSE(10.82,0,.1)+0*Vol_duod*ka du
ليا
    OUTFLOWS:
duo_secretion = PULSE(10.82,0,.1)
Ξ
    serosal_ill(t) = serosal_ill(t - dt) + (Adsorpt_ill - ile_secretion) * dt
<u>ļ</u>
INIT serosal ill = 0
T.
فإ
    INFLOWS:
    Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka_il
    OUTFLOWS:
    ile\_secretion = PULSE(1.50,0,.1)
    serosal_jej(t) = serosal_jej(t - dt) + (Adsorp_jej - jej_secretion) * dt
    INIT serosal jej = 0
    INFLOWS:
    Adsorp_jej = PULSE(15.76,0,1) + 0*Vol_jej*ka_je
   OUTFLOWS:
   jej\_secretion = PULSE(2.67,0,.1)
   serosal\_sto(t) = serosal\_sto(t - dt) + (Adsorp\_Stom - Stom\_Secretion) * dt
   INIT serosal sto = 0
   INFLOWS:
   Adsorp_Stom = 0*Vol stom*ka sd
```

```
OUTFLOWS:
     Stom Secretion = PULSE(16.67,0..1)
    Stomach(t) = Stomach(t - dt) + (-SD trans - stom ka) * dt
     INIT Stomach = 1000
    OUTFLOWS:
    SD_trans = if Stomach > 0 then kf_sd*Stomach else 0
    stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
    ELSE Vol_stom*sol_profile*SA_stom*perm_stom*3600
    total\_drug\_absorbed(t) = total\_drug\_absorbed(t - dt) + (tot\_abs\_rate) * dt
    INIT total drug absorbed = 0
    INFLOWS:
    tot_abs_rate = stom_ka+duo_ka+Jej_ka+Il_ka+colon ka 5
    Total_Elimination(t) = Total_Elimination(t - dt) + (elimination) * dt
    INIT Total_Elimination = 0
9
    INFLOWS:
    elimination = amt plasma*k elim
    Vol\_colon(t) = Vol\_colon(t - dt) + (vol\_ij + col\_secretion - vol\_cw - Adsorp\_col) * dt
    INIT Vol colon = 0
UT
INFLOWS:
    vol ij = Vol ileum*ka ic
\sqsubseteq col_secretion = 0
<u></u>
OUTFLOWS:
vol_cw = Vol_colon*ka col
Adsorp_col = PULSE(1.67,0,.1)+0*Vol_colon*ka_co
Vol_duod(t) = Vol_duod(t - dt) + (vol_sd + duo_secretion - voil_dj - Adsorp_Duo) * dt
   INIT Vol_duod = 0
   INFLOWS:
   vol_sd = kf_sd*Vol_stom
   duo_secretion = PULSE(10.82,0,.1)
   OUTFLOWS:
   voil_dj = Vol_duod*ka dj
   Adsorp\_Duo = PULSE(10.82,0,.1) + 0*Vol\_duod*ka du
   Vol_ileum(t) = Vol_ileum(t - dt) + (vol_ji + ile_secretion - Adsorpt_ill - vol_ij) * dt
   INIT Vol ileum = 0
   INFLOWS:
   vol_ji = Vol_jej*ka ji
   ile_secretion = PULSE(1.50.0.1)
```

```
OUTFLOWS:
     Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka il
     vol ij = Vol_ileum*ka_ic
     Vol_jej(t) = Vol_jej(t - dt) + (voil_dj + jej_secretion - vol_ji - Adsorp_jej) * dt
     INIT Vol jej = 0
     INFLOWS:
     voil dj = Vol duod*ka di
    jej\_secretion = PULSE(2.67,0,1)
    OUTFLOWS:
    vol_ji = Vol_jej*ka ji
    Adsorp jej = PULSE(15.76,0,1)+0*Vol jej*ka_je
    Vol\_stom(t) = Vol\_stom(t - dt) + (Stom\_Secretion - vol\_sd - Adsorp\_Stom) * dt
    INIT Vol_stom = PULSE(8.33,0,.1)
    INFLOWS:
    Stom_Secretion = PULSE(16.67,0,.1)
ū
ū
    OUTFLOWS:
Ð
    vol_sd = kf sd*Vol stom
iii
    Adsorp_Stom = 0*Vol_stom*ka_sd
Ш
    conc_plasma = (amt_plasma/volume)*mg_to_ug
Ш
    k12 = .839
    k21 = .67
#
    ka co = 1
    ka col = 3
ka_dj = 3
    ka_du = 1
   ka ic = 3
   ka il = 8.83
    ka_je = 1
   ka ii = 3
   ka sd = 1
   kf sd = 2.8
   k elim = .161
   mg_to_ug = 1000
   perm_colon = 3.80e-6
   perm_duo = 1.10e-6
   perm Il = 4.06e-6
   perm_{jej} = 2.17e-6
   perm stom = 1.10e-6
   ph_s = 1.5
   ph_s_2 = 6.6
   ph_s_3 = 6.6
```

```
ph_s_4 = 7.5
         ph_s_5 = 6.6
         SA colon = 138
         SA duo = 125
         SA II = 102
         SA \text{ jej} = 182
         SA stom = 50
         volume = 4*19200
       sol_profile = GRAPH(ph s)
     (1.\overline{00}, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65
       3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
       (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
       sol profile_2 = GRAPH(ph s 2)
     (1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), 
     3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
     (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
     sol_profile_3 = GRAPH(ph s 3)
   (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50,
   3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
   (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
   sol_profile_4 = GRAPH(ph_s_4)
  (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3
  3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
 (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
  sol_profile_5 = GRAPH(ph s 5)
 (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3
 3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
```

Appendix 3: Abbreviation Key For GI Model

The legend/key has been divided into sub-sections corresponding to the sub-sections of the model diagram.

Numbered suffixes (1, 2, 3, 4, 5, 6) have been assigned to distinguish between intestinal regions (stomach, duodenum, jejunum, ileum, colon, and waste, respectively).

- 1 stomach
- 2 duodenum
- 3 jejunum
- 4 ileum
- 5 colon
- 6 waste

For example, VOL 1 is the volume in the stomach, MASS 3 is the insoluble mass in the jejunum. In the equations, COMP 1 indicates the stomach, COMP 2 the duodenum, COMP 3, the jejunum, etc.

Ghosts are listed under the sub-section containing the original reservoir, flow regulator, or converter.

Abbreviations listed in italics are regionally dependent and set up as arrays to allow independent values for each intestinal region.

In general, ADJ as a prefix indicates a calculated parameter value (ADJ = adjusted), while ADJ as a suffix indicates an adjustment parameter (ADJ = adjustment).

Intestinal model

Reservoirs/Compartments

VOL ABS Fluid volume absorbed

VOL Fluid volume

C REL Mass of drug contained with a formulation or controlled release

device

MASS Insoluble mass of drug (not contained within the formulation or

controlled release device)

SOL Soluble mass of drug

ABSORPTION Mass of drug absorbed

Flow regulators

₫ Ø Ш ū M Ш Ξ

REABS VOL OUT CR OUT

Rate of water absorption Fluid volume transit rate

Formulation or controlled release device transit rate

CR INPUT

Drug release rate from formulation or controlled release device

MASS OUT

Insoluble drug mass transit rate

DISS PRECIP SOL OUT

Dissolution rate Soluble drug mass transit rate

FLUX

Absorption rate

ADJ PARMS (Adjustment Parameters)

VOL ADJ

Fluid volume absorption adjustment parameter

DISS ADJ TRANSIT ADJ

Dissolution rate adjustment parameter Transit time adjustment parameter

SA ADJ

Surface area adjustment parameter

FLUX ADJ EFFLUX ADJ CARRIER ADJ

Passive Absorption adjustment parameter Efflux or secretion adjustment parameter Active absorption adjustment parameter

PARMS (Parameters)

VOL PARM

Fluid volume absorption rate constant Surface area available for absorption

SURFACE AREA DOSE

The administered dose of drug

INIT VOLUME

The administered volume of water or fluid

TIME IN HOURS

A clock

pН

The physiological pH value

PARACELLULAR

A user controlled switch used to adjust absorption based on

absorption mechanism

TRANSIT TIME

TRANSFERS **CUMU TT**

GI transit rate constant Cumulative transit time

ADJ TRANSIT TIME

Adjusted GI transit time incorporating adjustment parameter and

user input

USER TT INPUT

User controlled adjustments to the GI transit time

OUTPUT CALCULATIONS

ABSORBED TOTAL

Total mass of drug absorbed (sum of ABSORPTION 1...5)

ű Ī Ō o M Ш Ŧ

FDp% Fraction or the dose absorbed into portal vein x 100

FLUX TOTAL Total absorption rate (sum of FLUX 1...5)

CUM DISS Cumulative drug mass dissolved

CR Release Cumulative drug mass released from formulation

CUM DISS RATE Sum of DISS PRECIP 1...5 CR cumrate Summ of CR INPUT 1 5

PERMEABILITY CALCULATION

ADJ PERM Adjusted permeability ncorporating all transport mechanisms and

relevant adjustment parameters

ACT PE Active or carrier-mediated absorptive permeability

Km Constant from the Michaelis-Mentin type permeability equation for

active transport

REGIONAL Passive permeability after regional correlation calculation (same as

PASS PE if regional correlation is not used)

PASS PE Passive permeability entered by user

RC A logical function used in determining the regional correlation A logical function used in determining the regional correlation RCSUM

SOLUBILITY CALCULATION

USER pH User supplied pH value for which a solubility value is available USER SOLUB User supplied solubility value corresponding to the USER pH value Solubility calculated (if necessary) at the appropriate pH value ADJ SOLUB

using the entered USER pH and USER SOLUB values

CONTROLLED RELEASE CALCULATION

CR RATE The instantaneous release rate from the formulation CR DOSE The total dose contained with the formulation CR AT TIME The cumulative drug mass release profile CR AT LAST The cumulative drug mass release profile

Note: CR AT TIME holds the value at the current time value (t), CR AT LAST holds the value at the immediately preceeding time value (t-1)

CONC CALCULATION

CONCENTRATIONS The dissolved drug concentration

DISSOLUTION CALCULATION

PRECIP Precipitation rate constant DISSOL Dissolution rate constant

ADJ DISS PRECIP Adjusted rate constant incorporating PRECIP, DISSOL and calculated concentration

Appendix 4: Equations, Parameters and Values For GI Model

```
面: ADJ PARMS
          CARRIER_ADJ[COMPS] = 0
            DISS_ADJ[COMP_1] = 1
 5
            DISS_ADJ[COMP 2] = 1
            DISS_ADJ[COMP_3] = 1
            DISS\_ADJ[COMP\_4] = 1
            DISS_ADJ[COMP_5] = 1
        EFFLUX_ADJ[COMPS] = 1
FLUX_ADJ[COMP_1] = 1
FLUX_ADJ[COMP_2] = 10
           EFFLUX_ADJ[COMPS] = 1
        FLUX_ADJ[COMP_3] = 8

FLUX_ADJ[COMP_4] = 2

FLUX_ADJ[COMP_5] = 1

SA_ADJ[COMP_1] = 1
10
            SA\_ADJ[COMP\_2] = 1
            SA_ADJ[COMP 3] = 1
SA\_ADJ[COMP 4] = 1
ā
           SA\_ADJ[COMP 5] = 1
印
            TRANSIT_ADJ[COMP 1] = 1
o
U
           TRANSIT_ADJ[COMP_2] = 1
Ш
           TRANSIT_ADJ[COMP_3] = 1
TRANSIT_ADJ[COMP_4] = 1
Ξ
           TRANSIT_ADJ[COMP 5] = 1
|
           VOL_ADJ[COMP_1] = 1
!
           VOL_ADJ[COMP_2] = 1
ΠJ
           VOL_ADJ[COMP 3] = 1
ä
           VOL\_ADJ[COMP\_4] = 1
        VOL_ADJ[COMP 5] = 1
        CONC CALCULATION
        CONCENTRATIONS[COMP_1] = if VOL_1=0.0 then 0 else if
           ADJ_SOLUB[COMP_1]<SOL_1/VOL_1 then ADJ_SOLUB[COMP_1] else SOL_1/VOL_1 +
            0°(SOL_2+SOL_5+SOL_3+SOL_4+VOL_3+VOL_2+VOL_4+VOL_5)
        CONCENTRATIONS[COMP_2] = if VOL_2 = 0.0 then 0 else if (VOL_2<1e-6 AND SQL 2<1e-7)
           then 0 else if ADJ_SOLUB[COMP_2]<SOL_2/VOL_2 then ADJ_SOLUB[COMP_2] else
            SOL_2NOL_2
           +0°(SOL_1+SOL_5+SOL_3+SOL_4+VOL_3+VOL_1+VOL_5+VOL_4)
        CONCENTRATIONS[COMP_3] = if VOL_3 = 0.0 then 0 else if (VOL_3<1e-6 AND SOL_3<1e-7)
           then 0 else if ADJ_SOLUB[COMP_3]<SOL_3/VOL_3 then ADJ_SOLUB[COMP_3] else
           SOL 3/VOL 3
           +0*(SOL_1+SOL_2+SOL_4+SOL_5+VOL_5+VOL_4+VOL_1+VOL_2)
        CONCENTRATIONS[COMP_4] = if VOL_4 = 0.0 then 0 else if (VOL_4 < 1e-6) AND SOL 4 < 1e-7
           then 0 else if ADJ_SOLUB[COMP_4]<SOL_4/VOL_4 then ADJ_SOLUB[COMP_4] else
           SOL_4/VOL_4
           +0*(SOL_1+SOL_2+SOL_3+SOL_5+VOL_1+VOL_2+VOL_3+VOL_5)
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CONCENTRATIONS[COMP_5] = if VOL_5 = 0.0 then 0 else if (VOL_5<1e-6 AND SOL_5<1e-7)
                       then 0 else if ADJ_SOLUB[COMP_5]<SOL_5/VOL_5 then ADJ_SOLUB[COMP_5] else
                       SOL 5/VOL 5
                       +0*(SOL_1+SOL_4+SOL_3+SOL_2+VOL_3+VOL_1+VOL_2+VOL_4)
CONTROL RELEASE CALCULATION
          CR_DOSE = 0
CR_RATE = (CR_AT_TIME-CR_AT
CR_AT_LAST = GRAPH(TIME-DT)
                      CR_DOSE = 0
                      CR_RATE = (CR_AT_TIME-CR_AT_LAST)*20*(CR_DOSE/100)
                      (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75,
                      66.1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6),
                      (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), 
                      79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9),
                      (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25,
                      80.0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0),
                     (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0,
                      80.0)...
         CR_AT_TIME = GRAPH(TIME)
                     (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75,
                     66.1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6),
                     (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), (5.50, 79.6), 
                     79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9),
                     (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), (9.00, 80.0), 
                     80.0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0),
                    (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0,
                    80.0)...
         DISSOLUTION CALCULATION
                   ADJ_DISS_PRECIP[COMP_1] = if VOL_1=0 then 0 else if
                   (SOL_1/VOL_1<ADJ_SOLUB[COMP_1]) then
                   (DISSOL[COMP_1]*DISS_ADJ[COMP_1]*MASS_1*(ADJ_SOLUB[COMP_1]-SOL_1/VOL_1)) else
                   ((SOL_1/VOL_1)-ADJ_SOLUB[COMP_1])*PRECIP[COMP_1]+
                   0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
                   OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
       ADJ_DISS_PRECIP[COMP_2] = if VOL_2=0 then 0 else if
                   (SOL_2/VOL_2<ADJ_SOLUB[COMP_2]) then
                   (DISSOL[COMP_2]*DISS_ADJ[COMP_2]*MASS_2*(ADJ_SOLUB[COMP_2]-SOL_2/VOL_2)) else
                   ((SOL_2/VOL_2)-ADJ_SOLUB[COMP_2])*PRECIP[COMP_2]
                   +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
                   OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
     ADJ_DISS_PRECIP[COMP_3] = if VOL_3=0 then 0 else if
                  (SOL_3/VOL_3<ADJ_SOLUB[COMP_3]) then
                  (DISSOL[COMP_3]*DISS_ADJ[COMP_3]*MASS_3*(ADJ_SOLUB[COMP_3]-SOL_3/VOL_3)) else
                  ((SOL_3/VOL_3)-ADJ_SOLUB[COMP_3])*PRECIP[COMP_3]
                  +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
```

OL_1+VOL_2+VOL_3+VOL_4+VOL_5)

```
ADJ_DISS_PRECIP[COMP_4] = if VOL_4=0 then 0 else if
      (SOL 4/VOL_4<ADJ_SOLUB[COMP_4]) then
      (DISSOL[COMP_4]*DISS_ADJ[COMP_4]*MASS_4*(ADJ_SOLUB[COMP_4]-SOL_4/VOL_4)) else
      ((SOL_4/VOL_4)-ADJ_SOLUB[COMP_4])*PRECIP[COMP_4]
      +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
       OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
   ADJ_DISS_PRECIP[COMP_5] = if VOL_5=0 then 0 else if
      (SOL_5/VOL_5<ADJ_SOLUB[COMP_5]) then
      (DISSOL[COMP_5]*DISS_ADJ[COMP_5]*MASS_5*(ADJ_SOLUB[COMP_5]-SOL_5/VOL_5)) else
      ((SOL_5/VOL_5)-ADJ_SOLUB[COMP_5])*PRECIP[COMP_5]
      +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
      OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
   DISSOL[COMP_1] = 1
      DISSOL[COMP 2] = 1
      DISSOL[COMP 3] = 1
      DISSOL[COMP 4] = 1
     DISSOL[COMP_5] = 1
      PRECIP[COMP_1] = 10
PRECIP[COMP_2] = 10
      PRECIP[COMP_3] = 10
      PRECIP[COMP 4] = 10
      PRECIP[COMP_5] = 10
   INPUTS
   INTESTINAL MODEL
  ABSORPTION_1(t) = ABSORPTION_1(t - dt) + (FLUX_1) * dt
      INIT ABSORPTION 1 = 0
ä
      INFLOWS:
ΠJ

⇒ FLUX_1 =
#
            CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
ABSORPTION_2(t) = ABSORPTION_2(t - dt) + (FLUX_2) * dt
      INIT ABSORPTION_2 = 0
      INFLOWS:
        충 FLUX_2 =
           CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
  \square ABSORPTION_3(t) = ABSORPTION_3(t - dt) + (FLUX_3) * dt
      INIT ABSORPTION 3 = 0
      INFLOWS:

⇒ FLUX_3 =
           CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
  ABSORPTION_4(t) = ABSORPTION_4(t - dt) + (FLUX_4) * dt
      INIT ABSORPTION_4 = 0
      INFLOWS:
```

```
☆ FLUX_4 =
             CONCENTRATIONS[COMP_4]*ADJ_PERM[COMP_4]*SURFACE_AREA[COMP_4]
   ABSORPTION_5(t) = ABSORPTION_5(t - dt) + (FLUX 5) * dt
       INIT ABSORPTION_5 = 0
       INFLOWS:

⇒ FLUX_5 = if time<32 then
</p>
            CONCENTRATIONS[COMP_5]*ADJ_PERM[COMP_5]*SURFACE_AREA[COMP_5]*(32-ti
             me)/48*(VOL 5/17.2) else 0
   C_REL_1(t) = C_REL_1(t - dt) + (- CR_OUT_1 - CR_INPUT_1) * dt
       INIT C_REL_1 = CR_DOSE
       OUTFLOWS:
         ⇔ CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0
         CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE
     C_REL_2(t) = C_REL_2(t - dt) + (CR_OUT_1 - CR_OUT_2 - CR_INPUT_2) * dt
      INIT C REL 2 = 0
       INFLOWS:

☆ CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0

ū
       OUTFLOWS:
⇔ CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0
₫
         증 CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE
₽
C_REL_3(t) = C_REL_3(t - dt) + (CR_OUT_2 - CR_OUT_3 - CR_INPUT_3) * dt
      INIT C REL 3 = 0
Ш
       INFLOWS:
Ш
         CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0
▙
       OUTFLOWS:
#

☆ CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0

ΠJ
         CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE
  C_REL_4(t) = C_REL_4(t - dt) + (CR_OUT_3 - CR_OUT_4 - CR_INPUT_4) * dt
      INIT C_REL_4 = 0
       INFLOWS:
        CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0
       OUTFLOWS:
        ⇔ CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0
        ♣ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE
  C_REL_5(t) = C_REL_5(t - dt) + (CR_OUT_4 - CR_OUT_5 - CR_INPUT_5) * dt
      INIT C_REL_5 = 0
       INFLOWS:
        CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0
       OUTFLOWS:
        CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0
        ☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE
  \square C_REL_6(t) = C_REL_6(t - dt) + (CR_OUT_5) • dt
      INIT C REL 6 = 0
      INFLOWS:
        * CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0
```

```
MASS_1(t) = MASS_1(t - dt) + (CR_INPUT_1 - MASS_OUT_1 - DISS_PRECIP_1) * dt
    INIT MASS_1 = DOSE
    INFLOWS:
      승 CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE
     OUTFLOWS:

★ MASS_OUT_1 = MASS_1*TRANSFERS[COMP_1]

⇒ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]

MASS_2(t) = MASS_2(t - dt) + (MASS_OUT_1 + CR_INPUT_2 - MASS_OUT_2 -
    DISS_PRECIP_2) * dt
    INIT MASS 2 = 0
    INFLOWS:

★ MASS_OUT_1 = MASS_1*TRANSFERS[COMP 1]

★ CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE

    OUTFLOWS:
      MASS_OUT_2 = MASS_2*TRANSFERS[COMP 2]

⇒ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP 2]

MASS_3(t) = MASS_3(t - dt) + (CR_INPUT_3 + MASS_OUT_2 - MASS_OUT_3 -
    DISS_PRECIP_3) * dt
    INIT MASS_3 = 0
    INFLOWS:

★ CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE

      ★ MASS_OUT_2 = MASS_2*TRANSFERS[COMP 2]
    OUTFLOWS:
      常 MASS_OUT_3 = MASS_3*TRANSFERS[COMP 3]
      ⇒ DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP 3]
MASS_4(t) = MASS_4(t - dt) + (CR_INPUT_4 + MASS_OUT_3 - MASS_OUT_4 -
   DISS_PRECIP_4) * dt
   INIT MASS_4 = 0
    INFLOWS:

★ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE

      MASS_OUT_3 = MASS_3*TRANSFERS(COMP 3)
    OUTFLOWS:
      MASS_OUT_4 = MASS_4*TRANSFERS[COMP 4]

⇒ DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]

MASS_5(t) = MASS_5(t - dt) + (CR_INPUT_5 + MASS_OUT_4 - MASS_OUT_5 -
   DISS PRECIP 5) * dt
   INIT MASS 5 = 0
    INFLOWS:
      ☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE

★ MASS_OUT_4 = MASS_4*TRANSFERS[COMP_4]

    OUTFLOWS:
      ☆ MASS_OUT_5 = if time>4 then MASS_5*TRANSFERS[COMP_5] else 0

⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP_5]

\square MASS_6(t) = MASS_6(t - dt) + (MASS_OUT_5) * dt
   INIT MASS 6 = 0
    INFLOWS:
```

```
★ MASS_OUT_5 = if tim >4 th n MASS_5*TRANSFERS[COMP_5] else 0
   SOL_1(t) = SOL_1(t - dt) + (DISS_PRECIP_1 - SOL_OUT_1 - FLUX_1) * dt
       INIT SOL_1 = 0
        INFLOWS:

☆ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]

        OUTFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP 1]

⇒ FLUX 1 =
             CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
   \square SOL_2(t) = SOL_2(t - dt) + (SOL_OUT_1 + DISS_PRECIP_2 - SOL_OUT_2 - FLUX_2) * dt
       INIT SOL 2 = 0
       INFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP 1]

         ⇒ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP_2]
        OUTFLOWS:

⇒ SOL_OUT_2 = SOL_2*TRANSFERS[COMP_2]

→ FLUX 2 = 
₫
             CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
面
Ð
      SOL_3(t) = SOL_3(t - dt) + (DISS_PRECIP_3 + SOL_OUT_2 - SOL_OUT_3 - FLUX_3) + dt
Ü
       INIT SOL_3 = 0
Ш
Ш
       INFLOWS:
≘
         DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP_3]
<u>ļ</u>

☆ SOL_OUT_2 = SOL_2*TRANSFERS[COMP 2]

H
       OUTFLOWS:
N
         SOL_OUT_3 = SOL_3*TRANSFERS[COMP_3]
خط

⇒ FLUX_3 = 
CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
≟
  \square SOL_4(t) = SOL_4(t - dt) + (DISS_PRECIP_4 + SOL_OUT_3 - SOL_OUT_4 - FLUX_4) + dt
      INIT SOL_4 = 0
       INFLOWS:

      ⇒ DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]

⇒ SOL_OUT_3 = SOL_3*TRANSFERS(COMP 3)

       OUTFLOWS:

⇒ SOL_OUT_4 = SOL_4*TRANSFERS[COMP_4]

⇒ FLUX 4 = 
            CONCENTRATIONS[COMP_4]*ADJ_PERM[COMP_4]*SURFACE_AREA[COMP_4]
  SOL_5(t) = SOL_5(t - dt) + (DISS_PRECIP_5 + SOL_OUT_4 - SOL_OUT_5 - FLUX_5) • dt
      INIT SOL 5 = 0
       INFLOWS:
```

```
⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP_5]

⇒ SOL_OUT_4 = SOL_4*TRANSFERS(COMP 4)

      OUTFLOWS:
        ⇒ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP_5] else 0

⇒ FLUX_5 = if time<32 then
</p>
           CONCENTRATIONS[COMP_5]*ADJ_PERM[COMP_5]*SURFACE_AREA[COMP_5]*(32-ti
           me)/48*(VOL_5/17.2) else 0
  \subseteq SOL_6(t) = SOL_6(t - dt) + (SOL_OUT_5) * dt
      INIT SOL 6 = 0
      INFLOWS:

☆ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP_5] else 0

  INIT VOL_1 = INIT_VOLUME
      OUTFLOWS:

⇒ REABS_1 = VOL_1*VOL_PARM[COMP_1]

        \bigcirc VOL_2(t) = VOL_2(t - dt) + (VOL_OUT_1 - VOL_OUT_2 - REABS 2) * dt
     INIT VOL 2 = 0
ū
      INFLOWS:
₽

☆ VOL_OUT_1 = VOL_1*TRANSFERS[COMP_1]

M
      OUTFLOWS:
ū

      ★ VOL_OUT_2 = VOL_2*TRANSFERS[COMP_2]

I
       REABS_2 = VOL_2*VOL_PARM[COMP_2]
VOL_3(t) = VOL_3(t - dt) + (VOL_OUT_2 - VOL_OUT_3 - REABS 3) * dt
     INIT VOL 3 = 0
Œ
      INFLOWS:
ļ.

      ★ VOL_OUT_2 = VOL_2*TRANSFERS[COMP 2]

N
      OUTFLOWS:
<u>___</u>

★ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

       REABS_3 = VOL_3*VOL_PARM[COMP_3]
INIT VOL 4 = 0
      INFLOWS:

⇒ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

      OUTFLOWS:

☆ VOL_OUT_4 = VOL_4*TRANSFERS[COMP_4]

       REABS_4 = VOL_4*VOL_PARM[COMP 4]
  \bigvee VOL_5(t) = VOL_5(t - dt) + (VOL_OUT_4 - VOL_OUT_5 - REABS_5) * dt
     INIT VOL 5=0
     INFLOWS:

★ VOL_OUT_4 = VOL_4*TRANSFERS[COMP_4]
     OUTFLOWS:

    Ö VOL_OUT_5 = VOL_5*TRANSFERS[COMP 5]
       REABS_5 = VOL_5*VOL_PARM[COMP_5]
 \bigvee VOL_6(t) = VOL_6(t - dt) + (VOL_OUT_5) • dt
     INIT VOL 6 = 0
```

```
INFLOWS:

⇒ VOL_OUT_5 = VOL_5*TRANSFERS[COMP_5]

      OL_ABS_1(t) = VOL_ABS_1(t - dt) + (REABS_1) * dt
        INIT VOL_ABS_1 = 0
        INFLOWS:
          REABS_1 = VOL_1*VOL_PARM[COMP_1]
    \bigvee VOL_ABS_2(t) = VOL_ABS_2(t - dt) + (REABS_2) • dt
        INIT VOL ABS 2 = 0
        INFLOWS:
          REABS_2 = VOL_2*VOL_PARM[COMP 2]
    \bigcirc VOL_ABS_3(t) = VOL_ABS_3(t - dt) + (REABS_3) * dt
       INIT VOL_ABS_3 = 0
        INFLOWS:
          REABS_3 = VOL_3*VOL_PARM[COMP 3]
    \bigcirc VOL_ABS_4(t) = VOL_ABS_4(t - dt) + (REABS_4) • dt
       INIT VOL ABS 4 = 0
        INFLOWS:

★ REABS_4 = VOL_4*VOL_PARM[COMP_4]

O
   o
       INIT VOL ABS 5 = 0
M
        INFLOWS:
ű
         REABS_5 = VOL_5*VOL_PARM[COMP 5]
Ш
    MULTI DOSE CALCULATION
   OUTPUT CALCULATIONS
   CR_Release(t) = CR_Release(t - dt) + (CR_cumrate) * dt
      . INIT CR_Release = 0
#
INFLOWS:
N
         CR_cumrate = CR_INPUT_1+CR_INPUT_2+CR_INPUT_3+CR_INPUT_4+CR_INPUT_5
=
   CUM_DISS(t) = CUM_DISS(t - dt) + (CUMM_DISS_RATE) * dt
       INIT CUM_DISS = 0
       INFLOWS:

★ CUMM_DISS_RATE = 
            DISS_PRECIP_1+DISS_PRECIP_2+DISS_PRECIP_3+DISS_PRECIP_4+DISS_PRECIP
   ○ ABSORBED_TOTAL = ABSORPTION_2+ABSORPTION_3+ABSORPTION_4+ABSORPTION_5
   FDp% = ABSORBED_TOTAL/DOSE*100
   FLUX_TOTAL = FLUX_2+FLUX_3+FLUX_4+FLUX_5
PARMS
   O DOSE = 1000
   INIT_VOLUME = 100PARACELLULAR = 1
      pH[COMP_1] = 1.5
      pH[COMP 2] = 5
      pH[COMP_3] = 6.5
```

```
pH[COMP_4] = 7
       pH[COMP_5] = 6.5
    SURFACE_AREA[COMP_1] = if PARACELLULAR =0 then 50*SA_ADJ[COMP_1] else
       50*SA_ADJ[COMP 1]
    SURFACE_AREA[COMP_2] = if PARACELLULAR=0 then 150*SA_ADJ[COMP_2] else
       7.5°SA_ADJ[COMP_2]
    SURFACE_AREA[COMP_3] = if PARACELLULAR=0 then 1000*SA_ADJ[COMP_3] else
       50*SA_ADJ[COMP 3]
    SURFACE_AREA[COMP_4] = if PARACELLULAR=0 then 1000*SA_ADJ[COMP_4] else
       50°SA_ADJ[COMP_4]
    SURFACE_AREA[COMP_5] = if PARACELLULAR=0 then 850*SA_ADJ[COMP_5] else
       42.5°SA_ADJ[COMP_5]
   TIME_IN_HOURS = TIME
     VOL_PARM[COMP_1] = 0*VOL_ADJ[COMP_1]
      VOL_PARM[COMP_2] = 0*VOL_ADJ[COMP_2]
VOL_PARM[COMP_3] = 1.75*VOL_ADJ[COMP_3]
      VOL_PARM[COMP_4] = 1.75*VOL_ADJ[COMP_4]
     VOL_PARM[COMP_5] = 0.10*VOL_ADJ[COMP_5]
   PERMEABILITY CALCULATION
    ACT_PE[COMPS] = [0.
U
       Ο.
L
       0,
لِنا
      0,
≅
      0]
   ADJ_PERM[COMP 1] =
      (2/(1+EFFLUX_ADJ[COMP_1]))*REGIONAL[COMP_1]*FLUX_ADJ[COMP_1]*3600+(CARRIER_
N
      DJ[COMP_1]*ACT_PE[COMP_1]*3600/(1+(CONCENTRATIONS[COMP_1]/(Km[COMP_1]))))*0
₩
  ADJ_PERM[COMP_2] =
      (2/(1+EFFLUX_ADJ[COMP_2]))*REGIONAL[COMP_2]*FLUX_ADJ[COMP_2]*3600+(CARRIER_
      DJ[COMP_2]*ACT_PE[COMP_2]*3600/(1+(CONCENTRATIONS[COMP_2]/(Km[COMP_2]))))
   ADJ_PERM[COMP 3] =
      (2/(1+EFFLUX_ADJ[COMP_3]))*REGIONAL[COMP_3]*FLUX_ADJ[COMP_3]*3600+(CARRIER_
      DJ[COMP_3]*ACT_PE[COMP_3]*3600/(1+(CONCENTRATIONS[COMP_3]/(Km[COMP_3]))))
  ADJ_PERM[COMP_4] =
      (2/(1+EFFLUX_ADJ[COMP_4]))*REGIONAL[COMP_4]*FLUX_ADJ[COMP_4]*3600+(CARRIER_
      DJ[COMP_4]*ACT_PE[COMP_4]*3600/(1+(CONCENTRATIONS[COMP_4]/(Km[COMP_4]))))
  ADJ_PERM[COMP 5] =
     (2/(1+EFFLUX_ADJ[COMP_5]))*REGIONAL[COMP_5]*FLUX_ADJ[COMP_5]*3600+(CARRIER_
     DJ[COMP_5]*ACT_PE[COMP_5]*3600/(1+(CONCENTRATIONS[COMP_5]/(Km[COMP_5]))))
```

```
( Km[COMPS] = [1 ,
       1,
       1,
   PASS_PE[COMPS] = [0 ,
       1.10E-06
       2.17E-06.
       4.06E-06.
       3.80E-061
   RC[COMP_1] = PASS_PE[COMP_1]*0
      RC[COMP_2] = IF PASS_PE[COMP_2]>0 THEN 1 ELSE 0
      RC[COMP_3] = IF PASS_PE[COMP_3]>0 THEN 2 ELSE 0
      RC[COMP_4] = IF PASS_PE[COMP_4]>0 THEN 4 ELSE 0
      RC[COMP_5] = PASS_PE[COMP_5]*0
   RCSUM = RC[COMP_2]+RC[COMP_3]+RC[COMP_4]
REGIONAL[COMP_1] = PASS_PE[COMP_1]+RCSUM*0
      REGIONAL[COMP_2] = if RCSUM=2 then
      (EXP( -9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_2]) -0.065515
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
Ū
      if RCSUM=4 then
I
Ш
      (EXP(-0.369414*LOGN(1/PASS_PE[COMP_4])+0.23756*LOGN(1/PASS_PE[COMP_4])^2-0.009
Ш
      9719*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
      if RCSUM=6 then
      0.5*(EXP( -9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_3]) -0.065515
ᆂ
N
      *LOGN(1/PASS_PE[COMP_3])^2))^(-1)
      +0.5°(EXP( -21.009845 + 4.544238 *LOGN(1/PASS_PE[COMP_4]) -0.140815
ᆂ
      *LOGN(1/PASS_PE[COMP_4])^2))^(-1) else
      PASS_PE[COMP_2]

    □ REGIONAL[COMP_3] = if RCSUM=1 then

      (EXP(-3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
      *LOGN(1/PASS_PE[COMP_2])^(-1) else
      if RCSUM=4 then
      (EXP(-0.093739*LOGN(1/PASS_PE[COMP_4])+0.182344*LOGN(1/PASS_PE[COMP_4])^2-0.00
      23631*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
      if RCSUM=5 then
     0.5°(EXP( -3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
     *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
     +0.5*(EXP( -15.415683 + 3.543563 *LOGN(1/PASS_PE[COMP_4]) -0.100318
     *LOGN(1/PASS_PE[COMP_4])^2))^(-1) eise
     PASS_PE[COMP 3]
```

```
REGIONAL[COMP_4] = if RCSUM=1 then
       (EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
       *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
       if RCSUM=2 then
       (EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
       *LOGN(1/PASS_PE[COMP_3])^2))^(-1) eise
       if RCSUM=3 then
       0.5*(EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
       *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
       +0.5*(EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
       *LOGN(1/PASS_PE[COMP_3])^2))^(-1) else
       PASS_PE[COMP_4]
    REGIONAL[COMP_5] = PASS_PE[COMP_5] +RCSUM*0
SOLUBILIY CALCULATION
   C ADJ_SOLUB[COMP_1] = if USER_pH[COMP_1]>=pH[COMP_1] then USER_SOLUB[COMP_1]
       else
       ((USER_SOLUB[COMP_2]-USER_SOLUB[COMP_1])/(USER_pH[COMP_2]-USER_pH[COMP_1]
))*(pH[COMP_1]-USER_pH[COMP_1])+USER_SOLUB[COMP_1]
   ADJ_SOLUB[COMP_2] = if USER_pH[COMP_2]=pH[COMP_2] then USER_SOLUB[COMP_2]
4
Ö
      else if USER_pH[COMP_2]<pH[COMP_2] then
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
Ō
      ))*(pH[COMP_2]-USER_pH[COMP_2])+USER_SOLUB[COMP_2] else
M
      ((USER_SOLUB[COMP_2]-USER_SOLUB[COMP_1])/(USER_pH[COMP_2]-USER_pH[COMP_1]
Ш
      ))*(pH[COMP_2]-USER_pH[COMP_1])+USER_SOLUB[COMP_1]
Ш
      ADJ_SOLUB[COMP_3] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
      else if USER_pH[COMP_3]<pH[COMP_3] then
((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
ᆂ
      ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
ΠIJ
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
1
      ))*(pH[COMP_3]-USER_pH[COMP_2])+USER_SOLUB[COMP_2]
ADJ_SOLUB[COMP_4] = if USER_pH[COMP_4]=pH[COMP_4] then USER_SOLUB[COMP_4]
      else if USER_pH[COMP_4]<pH[COMP_4] then
      ((USER_SOLUB[COMP_5]-USER_SOLUB[COMP_4])/(USER_pH[COMP_5]-USER_pH[COMP_4]
      ))*(pH[COMP_4]-USER_pH[COMP_4])+USER_SOLUB[COMP_4] else
      ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
      ))*(pH[COMP_4]-USER_pH[COMP_3])+USER_SOLUB[COMP_3]
  ADJ_SOLUB[COMP_5] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
      else if USER_pH[COMP_3]<pH[COMP_3] then
      ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
      ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
      ))*(pH[COMP_3]-USER_pH[COMP_2])+USER_SOLUB[COMP_2]
  USER_pH[COMPS] = [1.5,
      5.
     6.5.
     7,
     7.5]
```

```
USER_SOLUB[COMPS] = [31.
       3.65 .
      3.65,
      3.65.
      3.651
   TRANSIT TIME
      ADJ_TRANSIT_TIME[COMP_1] = .5*TRANSIT_ADJ[COMP_1]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_2] = .25*TRANSIT_ADJ[COMP_2]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_3] = 1.5*TRANSIT_ADJ[COMP_3]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_4] = 1.5*TRANSIT_ADJ[COMP_4]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_5] = 24*TRANSIT_ADJ[COMP_5]*USER_TT_INPUT
      CUMU_TT[COMP_1] = ADJ_TRANSIT_TIME[COMP_1]
      CUMU_TT[COMP_2] = ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]
CUMU_TT[COMP_3] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
3]
   CUMU_TT[COMP_4] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
П
      3]+ADJ_TRANSIT_TIME[COMP_4]
   CUMU_TT[COMP_5] =
Ш
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
      3]+ADJ_TRANSIT_TIME[COMP_4]+ADJ_TRANSIT_TIME[COMP_5]
TRANSFERS[COMP_1] = LOGN(10)ADJ_TRANSIT_TIME[COMP_1]
      TRANSFERS[COMP_2] = LOGN(10)ADJ_TRANSIT_TIME[COMP_2]
      TRANSFERS[COMP_3] = LOGN(10)ADJ_TRANSIT_TIME[COMP_3]
      TRANSFERS[COMP_4] = LOGN(10)ADJ_TRANSIT_TIME[COMP_4]
      TRANSFERS[COMP_5] = LOGN(10)ADJ_TRANSIT_TIME[COMP_5]
      USER_TT INPUT = 1
```